An immersed boundary method for simulating vesicle dynamics in three dimensions

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Outline

1. Introduction

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5. Future Works

What are Vesicles?

Vesicles are cellular organelles that are composed of a lipid bilayer.



Figure: Diagram of lipid vesicles showing a solution of molecules (green dots) trapped in the vesicle interior. (Taken from Wikipedia.org)

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Vesicle and Red Blood Cells (RBCs) both share similar mechanical behaviors.



Figure: Red Blood Cells (Taken from Google Search)

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Governing equations

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla \rho + \frac{1}{Re}\Delta \mathbf{u} + \mathbf{f}, \qquad (1)$$

$$\nabla \cdot \mathbf{u} = \mathbf{0},\tag{2}$$

$$\mathbf{f}(\mathbf{x}) = \int_{\Gamma} \left(\mathbf{F}_{\sigma} + \frac{1}{ReCa} \mathbf{F}_{b} \right) \delta(\mathbf{x} - \mathbf{X}(r, s, t)) \, \mathrm{d}A, \tag{3}$$

$$\mathbf{F}_{\sigma} = \nabla_{s}\sigma - 2H\sigma\mathbf{n}, \qquad \mathbf{F}_{b} = \frac{1}{2}\left(\Delta_{s}H + 2H(H^{2} - K)\right)\mathbf{n}, \qquad (4)$$

$$\frac{\partial \mathbf{X}}{\partial t}(r,s,t) = \mathbf{U}(r,s,t) = \int_{\Omega} \mathbf{u}(\mathbf{x},t) \delta(\mathbf{x} - \mathbf{X}(r,s,t)) d\mathbf{x}, \qquad (5)$$

$$\nabla_{\boldsymbol{s}} \cdot \boldsymbol{\mathsf{U}} = 0 \quad \text{on } \boldsymbol{\mathsf{\Gamma}}. \tag{6}$$

where $Re = \rho R_0^2 / \mu t_c$ (the Reynolds number), $Ca = \mu R_0^3 / c_b t_c$ (the capillary number), and $R_0 = \sqrt{A/4\pi} = (3V/4\pi)^{1/3}$ (effective radius).

$$\nu = \frac{3V}{4\pi (A/4\pi)^{3/2}}$$
(7)

The reduced volume ν represents the volume ratio between the vesicle and the sphere with the same surface area. ($\nu = 1$ for sphere), $\nu = 1$ for sphere), $\nu = 1$ for sphere).

Classical differential geometry

For the vesicle boundary X, define the first fundamental coefficients as

$$E = \mathbf{X}_r \cdot \mathbf{X}_r, \quad F = \mathbf{X}_r \cdot \mathbf{X}_s, \quad \text{and} \quad G = \mathbf{X}_s \cdot \mathbf{X}_s,$$

then

$$\nabla_s \sigma = \frac{G\mathbf{X}_r - F\mathbf{X}_s}{EG - F^2} \sigma_r + \frac{E\mathbf{X}_s - F\mathbf{X}_r}{EG - F^2} \sigma_s$$
$$\nabla_s \cdot \mathbf{U} = \frac{G\mathbf{X}_r - F\mathbf{X}_s}{EG - F^2} \cdot \mathbf{U}_r + \frac{E\mathbf{X}_s - F\mathbf{X}_r}{EG - F^2} \cdot \mathbf{U}_s$$

► Using a × (b × c) = (a · c)b - (a · b)c, we obtain two useful relations

$$\mathbf{X}_s imes \mathbf{n} = rac{G\mathbf{X}_r - F\mathbf{X}_s}{|\mathbf{X}_r imes \mathbf{X}_s|}, \quad \mathbf{n} imes \mathbf{X}_r = rac{E\mathbf{X}_s - F\mathbf{X}_r}{|\mathbf{X}_r imes \mathbf{X}_s|}$$

which give

$$\nabla_s \sigma = \frac{(\mathbf{X}_s \times \mathbf{n})\sigma_r + (\mathbf{n} \times \mathbf{X}_r)\sigma_s}{|\mathbf{X}_r \times \mathbf{X}_s|} \quad \text{and} \\ \mathbf{F} \quad \mathbf{X}_s \times \mathbf{n}_r + \mathbf{n}_s \times \mathbf{X}_r = -2H\mathbf{n}|\mathbf{X}_r \times \mathbf{X}_s|.$$

Nearly incompressible surface

To avoid solving the extra unknown tension $\sigma(r, s, t)$, we propose an alternative way to *approximate* the zero surface divergence. We use

$$rac{\partial}{\partial t} |\mathbf{X}_r imes \mathbf{X}_s| = (
abla_s \cdot \mathbf{U}) |\mathbf{X}_r imes \mathbf{X}_s|$$

from which each surface dilating factor should maintain the initial profile during time integration whenever $\nabla_s \cdot \mathbf{U} = 0$. Therefore, we introduce a spring-like elastic tension as

$$\sigma = \sigma_{0} \left(| \mathbf{X}_{r} imes \mathbf{X}_{s} | - | \mathbf{X}_{r}^{0} imes \mathbf{X}_{s}^{0} |
ight)$$

where $\sigma_0 \gg 1$ and $|\mathbf{X}_r^0 \times \mathbf{X}_s^0|$ is the initial surface dilating factor. We also define the modified elastic energy by

$$E_{\sigma}(\mathbf{X}) = \frac{\sigma_0}{2} \iint \left(|\mathbf{X}_r \times \mathbf{X}_s| - |\mathbf{X}_r^0 \times \mathbf{X}_s^0| \right)^2 drds.$$

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Derivation of the rate of change of surface dilation factor

$$\begin{split} \frac{\partial}{\partial t} |\mathbf{X}_r \times \mathbf{X}_s| &= \frac{\mathbf{X}_r \times \mathbf{X}_s}{|\mathbf{X}_r \times \mathbf{X}_s|} \cdot (\mathbf{X}_{rt} \times \mathbf{X}_s + \mathbf{X}_r \times \mathbf{X}_{st}) \\ &= \mathbf{n} \cdot (\mathbf{X}_{rt} \times \mathbf{X}_s) + \mathbf{n} \cdot (\mathbf{X}_r \times \mathbf{X}_{st}) \quad \left(\text{since } \mathbf{n} = \frac{\mathbf{X}_r \times \mathbf{X}_s}{|\mathbf{X}_r \times \mathbf{X}_s|}\right) \\ &= (\mathbf{X}_s \times \mathbf{n}) \cdot \mathbf{X}_{rt} + (\mathbf{n} \times \mathbf{X}_r) \cdot \mathbf{X}_{st} \quad (\text{using } (\mathbf{a} \times \mathbf{b}) \cdot \mathbf{c} = (\mathbf{b} \times \mathbf{c}) \cdot \mathbf{a}) \\ &= (\mathbf{X}_s \times \mathbf{n}) \cdot \mathbf{U}_r + (\mathbf{n} \times \mathbf{X}_r) \cdot \mathbf{U}_s \quad (\text{since } \mathbf{X}_t = \mathbf{U}) \\ &= \frac{G\mathbf{X}_r - F\mathbf{X}_s}{|\mathbf{X}_r \times \mathbf{X}_s|} \cdot \mathbf{U}_r + \frac{E\mathbf{X}_s - F\mathbf{X}_r}{|\mathbf{X}_r \times \mathbf{X}_s|} \cdot \mathbf{U}_s \quad (\text{using the two relations}) \\ &= (\nabla_s \cdot \mathbf{U}) |\mathbf{X}_r \times \mathbf{X}_s| \quad (\text{by the definition of } \nabla_s \cdot \mathbf{U}) \end{split}$$

Derivation of modified elastic force by variational derivative

$$\begin{aligned} \frac{d}{d\varepsilon} E_{\sigma}(\mathbf{X} + \varepsilon \mathbf{Y}) \Big|_{\varepsilon=0} \\ &= \iint \sigma_{0} \left(|\mathbf{X}_{r} \times \mathbf{X}_{s}| - |\mathbf{X}_{r}^{0} \times \mathbf{X}_{s}^{0}| \right) \frac{\mathbf{X}_{r} \times \mathbf{X}_{s}}{|\mathbf{X}_{r} \times \mathbf{X}_{s}|} \cdot \left(\mathbf{Y}_{r} \times \mathbf{X}_{s} + \mathbf{X}_{r} \times \mathbf{Y}_{s} \right) drds \\ &= \iint \sigma \mathbf{n} \cdot \left(\mathbf{Y}_{r} \times \mathbf{X}_{s} + \mathbf{X}_{r} \times \mathbf{Y}_{s} \right) drds \quad \left(\text{by } \mathbf{n} = \frac{\mathbf{X}_{r} \times \mathbf{X}_{s}}{|\mathbf{X}_{r} \times \mathbf{X}_{s}|} \right) \\ &= \iint \sigma(\mathbf{X}_{s} \times \mathbf{n}) \cdot \mathbf{Y}_{r} + \sigma(\mathbf{n} \times \mathbf{X}_{r}) \cdot \mathbf{Y}_{s} drds \quad (\text{by the scalar triple product formula}) \\ &= -\iint (\sigma \mathbf{X}_{s} \times \mathbf{n})_{r} \cdot \mathbf{Y} + (\sigma \mathbf{n} \times \mathbf{X}_{r})_{s} \cdot \mathbf{Y} drds \quad (\text{by integration by parts}) \\ &= -\iint [\sigma_{r} \mathbf{X}_{s} \times \mathbf{n} + \sigma_{s} \mathbf{n} \times \mathbf{X}_{r} + \sigma(\mathbf{X}_{s} \times \mathbf{n})_{r} + \sigma(\mathbf{n} \times \mathbf{X}_{r})_{s}] \cdot \mathbf{Y} drds \\ &= -\iint (\sigma_{r} \mathbf{X}_{s} \times \mathbf{n} + \sigma_{s} \mathbf{n} \times \mathbf{X}_{r} + \sigma \mathbf{X}_{s} \times \mathbf{n}_{r} + \sigma \mathbf{n}_{s} \times \mathbf{X}_{r}) \cdot \mathbf{Y} drds \\ &= -\iint (\nabla_{s} \sigma - 2\sigma H \mathbf{n}) \cdot \mathbf{Y} |\mathbf{X}_{r} \times \mathbf{X}_{s}| drds \\ &= -\int_{\Gamma} (\nabla_{s} \sigma - 2\sigma H \mathbf{n}) \cdot \mathbf{Y} dA \quad (\text{since } dA = |\mathbf{X}_{r} \times \mathbf{X}_{s}| drds) \\ &= -\int_{\Gamma} \mathbf{F}_{\sigma} \cdot \mathbf{Y} dA \end{aligned}$$

Grid layouts for Eulerian and Lagrangian variables



Figure: Fluid variables on a staggered MAC grid in 3D (left). Triangular surface patches that share the vertex X_k (right).

► The unit outward normal vector of the ℓ -th triangle is $\mathbf{n}_{\ell} = \frac{(\mathbf{x}_{\ell}^2 - \mathbf{x}_{\ell}^1) \times (\mathbf{x}_{\ell}^3 - \mathbf{x}_{\ell}^1)}{|(\mathbf{x}_{\ell}^2 - \mathbf{x}_{\ell}^1) \times (\mathbf{x}_{\ell}^3 - \mathbf{x}_{\ell}^1)|}.$

• The area of the ℓ -th triangle is $dA_{\ell} = \left| (\mathbf{X}_{\ell}^2 - \mathbf{X}_{\ell}^1) \times (\mathbf{X}_{\ell}^3 - \mathbf{X}_{\ell}^1) \right| / 2$.

Numerical algorithm

1. Compute the vesicle boundary forces.

We find the tension $\mathbf{F}_{\sigma}(\mathbf{X}_k) = \nabla_s \sigma(\mathbf{X}_k) - \sigma(\mathbf{X}_k) \mathbf{H}(\mathbf{X}_k)$ using $\sigma_{\ell} = \tilde{\sigma}_0 \left(\mathsf{d} A_{\ell} - \mathsf{d} A_{\ell}^0 \right)$, where formally $\tilde{\sigma}_0 = \sigma_0 / (\mathsf{d} r \mathsf{d} s)$, $\sigma(\mathbf{X}_k) = \sum \sigma_{\ell}/3,$ $\ell \in T(\mathbf{X}_{l})$ $\nabla_{s}\sigma_{\ell} = \frac{(\mathbf{X}_{\ell}^{3} - \mathbf{X}_{\ell}^{1}) \times \mathbf{n}_{\ell}}{2 \, \mathrm{d} \Delta_{s}} (\sigma_{\ell}^{2} - \sigma_{\ell}^{1}) + \frac{\mathbf{n}_{\ell} \times (\mathbf{X}_{\ell}^{2} - \mathbf{X}_{\ell}^{1})}{2 \, \mathrm{d} A_{\ell}} \left(\sigma_{\ell}^{3} - \sigma_{\ell}^{1}\right),$ $\nabla_{s}\sigma(\mathbf{X}_{k}) = \sum_{k=1,\dots,k} \omega_{\ell}\nabla_{s}\sigma_{\ell}, \text{ where } \omega_{\ell} = \frac{\mathrm{d}A_{\ell}/3}{\mathrm{d}A(\mathbf{Y}_{\ell})},$ $\ell \in T(\mathbf{X}_{\ell})$ $\mathbf{H}(\mathbf{X}_k) = \frac{1}{2 \, \mathrm{d} A(\mathbf{X}_k)} \sum_{\ell \in \mathcal{T}(\mathbf{X}_k)} \mathbf{n}_{\ell} \times (\mathbf{X}_{\ell}^3 - \mathbf{X}_{\ell}^2), \text{ where } \mathbf{H} = 2H\mathbf{n}.$

For a smooth surface patch *S*, the last formula is a discrete version of $\int_{S} 2H\mathbf{n} \, dA = \oint_{\partial S} \mathbf{n} \times d\mathbf{X}$, and equivalent to the cotangent formula.

From the discrete version of bending energy

$$E_b[\mathbf{X}] = \frac{c_b}{8} \sum_{k=1}^{N_v} |\mathbf{H}(\mathbf{X}_k)|^2 \, \mathrm{d}A(\mathbf{X}_k),$$

we obtain the bending force $F_b(X_k)dA(X_k) =$

$$\frac{c_b}{8} \sum_{\ell \in \mathcal{T}(\mathbf{X}_k)} \left(\left(H_{\ell} - \mathbf{n}_{\ell} \cdot \mathbf{C}_{\ell} \right) \left(\frac{1}{2} \mathbf{n}_{\ell} \times \mathbf{E}_{\ell}^k \right) + \frac{1}{2} \mathbf{C}_{\ell} \times \mathbf{E}_{\ell}^k + \mathbf{n}_{\ell} \times \mathbf{h}_{\ell}^k \right),$$

where

$$\begin{split} H_{\ell} &= \frac{1}{3} \sum_{p \in V(\ell)} |\mathbf{H}(\mathbf{X}_{p})|^{2}, \quad \mathbf{C}_{\ell} = \frac{1}{dA_{\ell}} \sum_{p \in V(\ell)} \mathbf{E}_{\ell}^{p} \times \mathbf{H}(\mathbf{X}_{p}), \\ \mathbf{E}_{\ell}^{k} &= \mathbf{X}_{\ell}^{3} - \mathbf{X}_{\ell}^{2}, \quad \mathbf{h}_{\ell}^{k} = \mathbf{H}(\mathbf{X}_{\ell}^{3}) - \mathbf{H}(\mathbf{X}_{\ell}^{2}). \\ \text{Thus, the boundary force becomes} \\ \mathbf{F}(\mathbf{X}_{k}^{n}) dA(\mathbf{X}_{k}^{n}) &= \mathbf{F}_{\sigma}(\mathbf{X}_{k}^{n}) dA(\mathbf{X}_{k}^{n}) + \mathbf{F}_{b}(\mathbf{X}_{k}^{n}) dA(\mathbf{X}_{k}^{n}). \end{split}$$

2. Solve the Navier-Stokes

$$\rho \left(\frac{3\mathbf{u}^* - 4\mathbf{u}^n + \mathbf{u}^{n-1}}{2\Delta t} + 2\left(\mathbf{u}^n \cdot \nabla_h\right)\mathbf{u}^n - \left(\mathbf{u}^{n-1} \cdot \nabla_h\right)\mathbf{u}^{n-1} \right)$$

= $-\nabla_h p^n + \mu \Delta_h \mathbf{u}^* + \sum_{k=1}^{N_v} \mathbf{F}(\mathbf{X}_k^n) \, dA(\mathbf{X}_k^n) \delta_h\left(\mathbf{x} - \mathbf{X}_k^n\right),$
 $\Delta_h p^* = \frac{3\rho}{2\Delta t} \nabla_h \cdot \mathbf{u}^*, \quad \frac{\partial p^*}{\partial \mathbf{n}} = 0 \text{ on } \partial\Omega, \quad \mathbf{u}^* = \mathbf{u}^{n+1} \text{ on } \partial\Omega,$
 $\mathbf{u}^{n+1} = \mathbf{u}^* - \frac{2\Delta t}{3\rho} \nabla_h p^*, \nabla_h p^{n+1} = \nabla_h p^* + \nabla_h p^n - \frac{2\mu\Delta t}{3\rho} \Delta_h(\nabla_h p^*).$

3. Update the new position

$$\mathbf{X}_{k}^{n+1} = \mathbf{X}_{k}^{n} + \Delta t \sum_{\mathbf{x}} \mathbf{u}^{n+1}(\mathbf{x}) \delta_{h}(\mathbf{x} - \mathbf{X}_{k}^{n}) h^{3}$$

Equivalence of the discrete mean curvature vector formula and the cotangent formula



Figure: The notations for the computation of the mean curvature vector using two equivalent formulas.

We begin with the cotangent formula

$$\mathbf{H}(\mathbf{X}) dA(\mathbf{X}) = \frac{1}{2} \sum_{j=1}^{N} \left(\cot \alpha_j + \cot \beta_j \right) (\mathbf{X} - \mathbf{X}_j),$$

where X_j are the vertices within 1-ring of the vertex X, and the angles α_j and β_j are the corresponding angles. The righthand side becomes

$$\begin{split} &\frac{1}{2}\sum_{j=1}^{N}\left(\cot\alpha_{j}+\cot\beta_{j}\right)\left(\mathbf{X}-\mathbf{X}_{j}\right)\\ &=-\frac{1}{2}\sum_{j=1}^{N}\cot\alpha_{j}(\mathbf{X}_{j}-\mathbf{X})+\cot\beta_{j}(\mathbf{X}_{j}-\mathbf{X})\\ &=-\frac{1}{2}\sum_{j=1}^{N}\cot\alpha_{j}(\mathbf{X}_{j}-\mathbf{X})+\cot\beta_{j-1}(\mathbf{X}_{j-1}-\mathbf{X}) \text{ (using the periodicity of index)}\\ &=-\frac{1}{2}\sum_{j=1}^{N}\cot\alpha_{j}(\mathbf{X}_{\ell}^{3}-\mathbf{X}_{\ell}^{1})+\cot\beta_{j-1}(\mathbf{X}_{\ell}^{2}-\mathbf{X}_{\ell}^{1}) \text{ (denoting the vertices in the }\ell\text{-th triangle})\\ &=-\frac{1}{2}\sum_{j=1}^{N}\cot\alpha_{j}\mathbf{X}_{31}+\cot\beta_{j-1}\mathbf{X}_{21}, \text{ (where }\mathbf{X}_{ij}=\mathbf{X}_{\ell}^{i}-\mathbf{X}_{\ell}^{j}). \end{split}$$

$$\tag{8}$$

Using the identity $\cot \theta = \frac{\mathbf{a} \cdot \mathbf{b}}{|\mathbf{a} \times \mathbf{b}|} = \frac{\mathbf{a} \cdot \mathbf{b}}{2 dA}$, where θ is the angle between the two vectors \mathbf{a} and \mathbf{b} , for the ℓ -th triangle with the vertices \mathbf{X}_{ℓ}^1 , \mathbf{X}_{ℓ}^2 , \mathbf{X}_{ℓ}^3 and its area dA_{ℓ} , we obtain

$$\cot \alpha_j = \frac{\mathbf{X}_{12} \cdot \mathbf{X}_{32}}{2 \, \mathrm{d} \mathcal{A}_\ell}, \quad \cot \beta_{j-1} = \frac{\mathbf{X}_{13} \cdot \mathbf{X}_{23}}{2 \, \mathrm{d} \mathcal{A}_\ell}.$$

Substituting these cotangents into Eq. (8) and summing all the triangles $T(\mathbf{X})$ within 1-ring around the vertex \mathbf{X} , we have

$$\frac{1}{2}\sum_{\ell\in\mathcal{T}(\mathbf{X})}\frac{(\mathbf{X}_{21}\cdot\mathbf{X}_{32})\mathbf{X}_{31}-(\mathbf{X}_{31}\cdot\mathbf{X}_{32})\mathbf{X}_{21}}{2\,\mathsf{d}A_\ell},$$

which, using the vector triple product $(a\times b)\times c=(a\cdot c)b-(b\cdot c)a,$ becomes

$$\begin{aligned} &\frac{1}{2}\sum_{\ell\in\mathcal{T}(\mathbf{X})}\frac{(\mathbf{X}_{21}\times\mathbf{X}_{31})\times\mathbf{X}_{32}}{2\,\mathrm{d}A_{\ell}} \\ &= &\frac{1}{2}\sum_{\ell\in\mathcal{T}(\mathbf{X})}\frac{(\mathbf{X}_{21}\times\mathbf{X}_{31})\times\mathbf{X}_{32}}{|\mathbf{X}_{21}\times\mathbf{X}_{31}|} \\ &= &\frac{1}{2}\sum_{\ell\in\mathcal{T}(\mathbf{X})}\mathbf{n}_{\ell}\times\mathbf{X}_{32} = \frac{1}{2}\sum_{\ell\in\mathcal{T}(\mathbf{X})}\mathbf{n}_{\ell}\times(\mathbf{X}_{\ell}^{3}-\mathbf{X}_{\ell}^{2}). \end{aligned}$$

Remesh of triangular surface



Figure: Re-meshing triangulation by edge addition (top) and deletion (bottom).

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Mapping of local area during simulation

$$\sigma_{\ell} = \tilde{\sigma}_0 \left(\mathsf{d} \mathsf{A}^t_{\ell} - \mathsf{d} \mathsf{A}^0_{\ell} \right)$$

X(0)





# Vertex	(x, y, z)	# Triangle	(v_1,v_2,v_3)	# Vertex	(x, y, z)
1	(0,0,0)	1	(1,2,3)	1	(0.1, 0, 0)
2	(0,0,1)	2	(1,4,5)	2	(0,0,2.1)
3	(0,1,1)	3	(1,6,7)	3	(1.2, 1, 2)
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Figure: Mapping of triangular area.

Numerical results

Numerical issues

- Accuracy check for mean curvature and bending force
- Study on different stiffness parameter $\tilde{\sigma_0}$
- Convergence of vesicle configuration and fluid velocity
- Numerical experiments
 - A suspended vesicle in quiescent flow
 - A vesicle in shear flow
 - A vesicle under the gravity

Numerical parameters

Unless otherwise stated, we use

- ▶ Re = 1, Ca = 50
- $\sigma_0 = 6 \times 10^5$, grid width h = 6/128
- The initial number of triangles is either 81920 or 327680

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Accuracy check for mean curvature and bending force

Using spherical parametric coordinates $(\theta, \phi) \in [0, 2\pi] \times [0, \pi]$,

- Unit sphere: $\mathbf{X}(\theta, \phi) = (\cos \theta \sin \phi, \sin \theta \sin \phi, \cos \phi)$,
- Ellipsoid: $\mathbf{X}(\theta, \phi) = (0.5 \cos \theta \sin \phi, 0.5 \sin \theta \sin \phi, \cos \phi),$
- ► Biconcave surface: $\mathbf{X}(\theta, \phi) = (\cos \theta \sin \phi, \sin \theta \sin \phi, (0.1242 + 0.8012 \sin^2 \phi 0.4492 \sin^4 \phi) \cos \phi).$



Figure: Left: A triangulated biconcave surface and its cross-sectional view. Right: The comparison of mean curvature between numerical values (symbols) and exact values (solid lines) for three different surfaces. Here, the number of vertices is $N_v = 2562$ corresponding to 5120 triangles used.



Figure: The L^2 errors for the mean curvature H (left) and the bending force $\mathbf{F}_b dA$ (right) as functions of the number of triangles.

The L^2 error of a function ψ is calculated as $\sqrt{\sum_{k=1}^{N_v} |\psi^e(\mathbf{X}_k) - \psi(\mathbf{X}_k)|^2 dA(\mathbf{X}_k)},$ where $\psi^e(\mathbf{X}_k)$ is the exact value and $\psi(\mathbf{X}_k)$ is the computed value.

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Study on different stiffness parameter $\tilde{\sigma_0}$

In this test, we study how the stiffness number $\tilde{\sigma}_0$ affects the conservation of surface area and vesicle volume, and the total surface energy.

- ▶ Put an initially oblate vesicle $X(\theta, \phi) = (\cos \theta \sin \phi, \sin \theta \sin \phi, \cos \phi/3.5)$ in quiescent flow
- Computational domain Ω = [-2,2]³ with grid size 128³
- Choose $\tilde{\sigma_0} = 6 \times 10^4, 6 \times 10^5, 6 \times 10^6$
- The meshwidth h = 1/32 and the time step size $\Delta t = h/16$
- The number of triangles used in the initial vesicle surface is 81920 with 40962 number of vertices.



Figure: The comparison for three different stiffness parameters: $\tilde{\sigma_0} = 6 \times 10^4 (\triangle), 6 \times 10^5 (\square)$, and $6 \times 10^6 (\bigcirc)$. (a) the maximum relative error of the local surface area; (b) the relative error of the global surface area; (c) the relative error of the global volume; (d) the total energy.

Convergence of vesicle configuration and fluid velocity

- Relax the same oblate vesicle with $\nu = 0.643$ in a cube $[-2, 2]^3$
- ▶ The grid size *N* = 32, 64, 128, 256
- $ilde{\sigma_0} = (N/32)^2 10^4$ and $\Delta t = h/8$
- $ratio = \log_2(\|u_N u_{2N}\|_{\infty} / \|u_{2N} u_{4N}\|_{\infty})$
- ▶ When N = 32, we use 5120 number of triangles which corresponds to 2562 number of vertices.



Figure: The ratios of convergence for the fluid velocity (u, v, w) and the vesicle configuration **X**. Left: N = 32; Right: N = 64

Numerical experiments

A suspended vesicle in quiescent flow

- Oblate surface: $X(\theta, \phi) = (\cos \theta \sin \phi, \sin \theta \sin \phi, \cos \phi/3.5)$
- Prolate surface: $X(\theta, \phi) = (0.2 \cos \theta \sin \phi, 0.2 \sin \theta \sin \phi, \cos \phi)$
- Oscillatory surface: X(θ, φ) = (³/₂₀ r(φ) cos θ sin φ, ³/₂₀ r(φ) sin θ sin φ, ³/₂₅ r(φ) cos φ), where r(φ) = √cos² φ + 9 sin² φ + cos²(4φ).

 Ω = [-2, 2]³, c_b = 0.02, σ₀ = 6 × 10⁵, and Δt = h/16



Figure: Suspended vesicles in quiescent flow. Oblate vesicle (two upper-left panels); Prolate vesicle (two upper-right panels); Oscillatory vesicle (lower panels)

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A vesicle in shear flow

- Put a prolate vesicle in a simple shear flow $\mathbf{u} = (z, 0, 0)$
- \blacktriangleright The non-dimensional shear rate $\chi=\mu R_0^3/c_b$
- $\Omega = [-3,3]^3$ and a small Reynolds number $Re = 10^{-3} \ll 1$ (Stokes flow regime)
- ▶ The reduced volume $\nu = 0.8$, 0.85, 0.9, 0.95, and 0.975 by fixing the effective radius $R_0 = 1$

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Figure: The simulation setup of a vesicle motion in a shear flow (top) and the tank-treading motion of a vesicle with $\nu = 0.8$ in a shear flow with $\chi = 100$ (bottom).

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Figure: The plot of the inclination angle (left) and the scaled mean angular velocity (right) as functions of reduced volume ν for different dimensionless shear rate χ .

► The frequency ω can be computed using $\omega = \frac{1}{N_v} \sum_{i=1}^{N_v} \frac{|\mathbf{r} \times \mathbf{v}|}{|\mathbf{r}|^2}$, where \mathbf{r} and \mathbf{v} are the position and velocity of the vertices projected on the *xz*-plane, respectively.



Figure: Tumbling motion of a vesicle with $\nu = 0.8$ and $\lambda = 40$ in a shear flow with $\chi = 100$. The computed time is up to t = 24.

To consider viscosity contrast between the interior and exterior of vesicle, instead of

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \frac{1}{Re}\Delta \mathbf{u} + \mathbf{f}, \qquad (9)$$

we use

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla \rho + \frac{1}{Re} \nabla \cdot \left[\mu(\mathbf{x}) \left(\nabla \mathbf{u} + \nabla \mathbf{u}^{T}\right)\right] + \mathbf{f}, \qquad (10)$$

where $\mu(\mathbf{x})$ is the dimensionless viscosity contrast.



Figure: The volume relative errors (left) and the surface area relative errors (right) for the cases of with or without the penalty volume conservation term Eq. (11). Here, $\nu = 0.8$ and $\chi = 100$. The viscosity contrast $\lambda = 1$ and $\lambda = 40$, respectively.

To conserve the vesicle volume, we add

$$\mathbf{F}_{\nu} \mathrm{d}A(\mathbf{X}) = -C_{\nu} \left(\frac{V^{t} - V^{0}}{V^{0}}\right) \mathbf{n} \, \mathrm{d}A(\mathbf{X}), \tag{11}$$

where C_v is a sufficiently large constant called a penalty parameter, V^t is the global volume of vesicle at time t, and V^0 is the global volume of initially given vesicle.

A vesicle under the gravity

- Prolate: $\mathbf{X}(\theta, \phi) = (0.5 \cos \theta \sin \phi, 0.5 \sin \theta \sin \phi, \cos \phi)$
- Oblate: $\mathbf{X}(\theta, \phi) = (0.75 \cos \theta \sin \phi, 0.75 \sin \theta \sin \phi, 0.375 \cos \phi)$
- ▶ The prolate vesicle is placed at different tilted angles $\eta = 0, \pi/4$ and $\pi/2$ initially to see how the initial orientation affects the equilibrium shape
- ► To model this problem, simply add an interfacial force $\mathbf{F}_{g} dA(\mathbf{X}) = (\rho^{i} - \rho^{e})(\mathbf{g} \cdot \mathbf{X}) dA(\mathbf{X})\mathbf{n}$ where ρ^{i} and ρ^{e} are interior and exterior fluid densities, respectively, and $\mathbf{g} = (0, 0, -1)$



Figure: The prolate vesicle with three different tilted angles $\eta = 0, \pi/4, \pi/2$ (first to third column) and oblate (fourth column) vesicle under the gravity. All the snapshots are taken at the same time.

Future Works

- High-order scheme to compute the curvatures and the Laplace-Beltrami operator
- Vesicle dynamics in extensional flow or in Poiseuille flow
- Multi-vesicle problems to mimic the behaviors of RBCs in capillary

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- Viscosity contrast effects on vesicle dynamics
- Reynolds number effects on vesicle dynamics

Thank you for your attention!

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